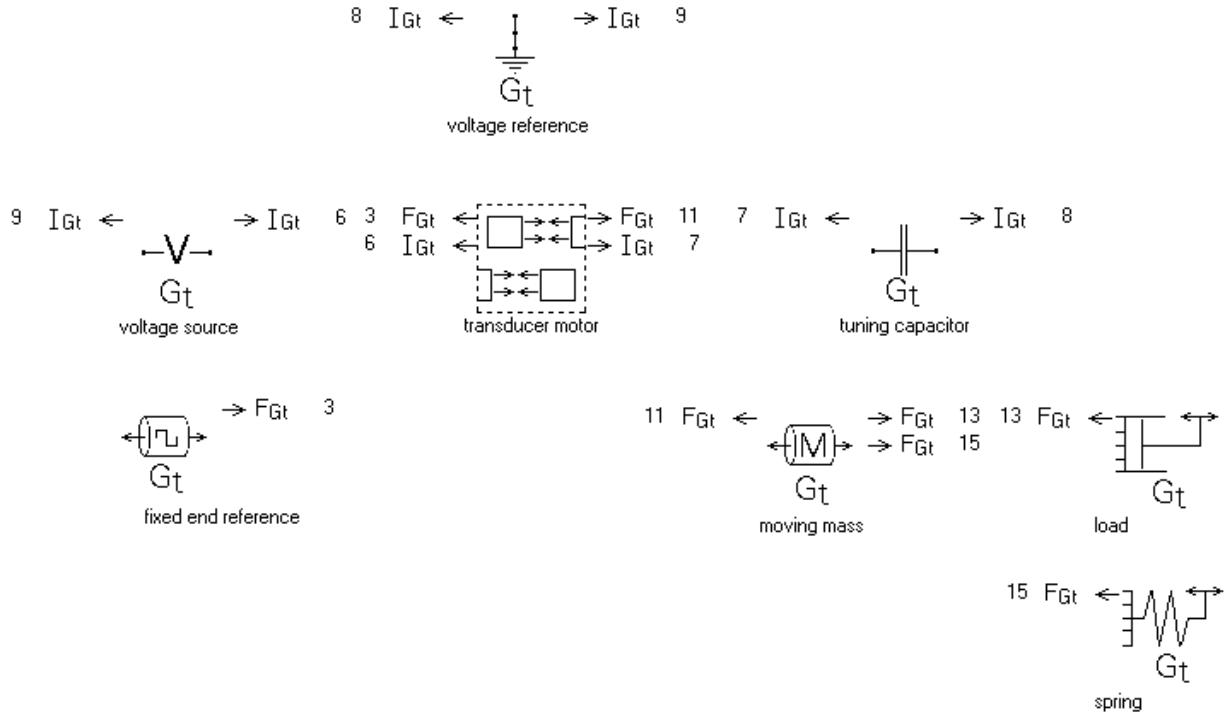


# Sage Model Notes

## MotorTransducer.stl

D. Gedeon  
18 October 2012

A model of a generic linear motor based on a non-physical transducer component that provides mechanical force in proportion to electrical current. The Sage model looks like this:



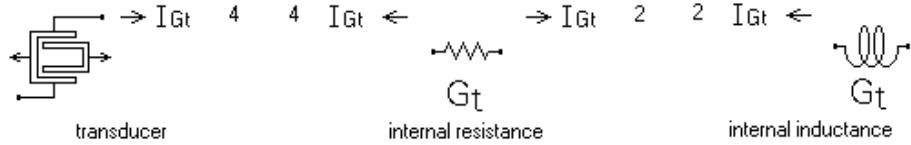
A *voltage source* (second row) drives electrical current through the components in the *transducer motor* submodel in series with a *tuning capacitor*. A constrained piston *fixed end reference* anchors the negative end of the transducer. The other end of the transducer drives the *moving mass* connected to a damper *load* and a *spring*. The driving voltage and phase are independent inputs and the electrical current through the circuit and motion of the *moving mass* are outputs.

One purpose of the *spring* is to establish the mean position of the *moving mass*. The *transducer* force depends only on the electrical current and the *load* force only on the mechanical velocity, neither of which care about the mean position. The presence of the *spring* prevents the *moving mass* mean position from drifting off to absurd values.

The purpose of the *tuning capacitor* is to adjust the voltage and current so they are in phase in the voltage source so as to transfer the most electrical power for a given voltage amplitude. In electrical engineering parlance the *tuning capacitor* adjusts the voltage source *power factor* to one. The optimizer chooses the tuning capacitance in this model by optimizing *tuning capacitor C* input in order to satisfy this constraint in the *voltage source*:

$$F_{\Delta V} \cdot Arg.1 = F_I \cdot Arg.1$$

The transducer motor submodel contains these components:



The transducer converts electrical current  $I$  to mechanical force  $F$  or vice-versa according to the linear relationship

$$F = C_f I$$

Where  $C_f$  is based on the inputs

|          |  |           |
|----------|--|-----------|
| $C_{f0}$ | force coefficient at $X = 0$ (N/A)           | 1.000E+02 |
| $X_m$    | reference extension (m)                      | 1.000E-02 |
| $R_p$    | force coef / $C_{f0}$ at $X = X_m$ (NonDim)  | 1.000E+00 |
| $R_n$    | force coef / $C_{f0}$ at $X = -X_m$ (NonDim) | 1.000E+00 |

Wired in series with the *transducer* are *internal resistance* and *internal inductance* components that capture some of the electrical properties of a real transducer (e.g. moving magnet motor). In particular the *internal resistance* dissipates electrical power that is not available as mechanical power output from the *transducer*.

**To model a linear alternator** you could replace the *moving mass*, *load* and *spring* by a constrained piston or just remove the *load* and apply a forcing function to the *moving mass*, either with the built-in FF input or through a force connection to another moving component of your model. Then replace the *voltage source* with a load resistor. The model would then convert mechanical power input from the driving piston to electrical power in dissipated in the load resistor.

## Energy Balance

Energy conservation is built into electrical and mechanical components separately and into the transducer component via the relationship between mechanical force  $F$ , relative velocity  $dx/dt$ , voltage drop  $\Delta V$  and current  $I$

$$F \frac{dx}{dt} = \Delta V I$$

This table summarizes the overall time-average energy balance:

|                                       | Power W    |
|---------------------------------------|------------|
| Input power from voltage source (Fwe) | -6.433E+01 |
| Internal resistance $I^2R$ loss (FWe) | 4.138E+00  |
| Load power dissipation (W)            | 6.019E+01  |

The motor efficiency is available a user-defined variable in the root model:

|                    |           |
|--------------------|-----------|
| Efficiency         | 9.357E-01 |
| WmechOut / WelecIn |           |

Where WmechOut and WelecIn are user-defined variables in the *transducer* and *voltage source* components.